

Go from H₂S to S in One Step: Use of Heteropoly Compound Solution as Efficient Absorbent and the Effect of Metal Sulfide Additive

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Abstract. A new liquid redox method for low sulfur containing gas (with H₂S concentration less than 1000mg/m³) treatment was developed employing the heteropoly compounds of molybdenum and phosphorus. The desulfurization characteristic of the absorbent system of H₄PVMo₁₁O₄₀ was investigated by dynamic outlet-gas H₂S concentration detection method. The absorbent system was found to have fairly good absorption-regeneration performance, with a H₂S removal rate of up to 100% in the presence of CuS, hence it is promising in pollution control and resource reclamation.

Keywords: hydrogen sulfide, desulfurization, liquid redox, absorption, heteropoly compound

1. Introduction

Hydrogen sulfide, as a highly undesirable contaminant existing in industrial gases, such as natural gas and coke oven gas, has long been confirmed to be hazardous material which should be removed to the possible lowest limit for reasons from both environmental restrictions and process requirements. Among the numerous H₂S removal approaches developed by now, liquid redox method has the remarkable advantage in that it can convert H₂S directly to elemental sulfur without causing secondary pollution [1,2]. Furthermore, the device it employed is that of conventional, which is quite economically acceptable compared to the well-known Claus apparatus for sulfur recovery. Recent concern for liquid redox method has been making iron chelate base absorbents the hot point. But iron chelate base absorbent is not as stable as desired, it may give rise to ferric sulfide by-product when reacting with H₂S, and there are also some difficulties in its regeneration, hence, the amendment of iron chelate base absorbent is still a problem. It is desirable to develop a new absorbent, good in chemical stability, easy of being regenerated, uncomplicated in composition and capable of oxidizing H₂S to elemental sulfur effectively. An innovative approach to liquid redox process involving the use of heteropoly compounds (HPC) appears to be a promising resolution to H₂S removal and sulfur recovery from industrial gases, to which a detailed introduction will be given in this presentation.

Being a kind of catalyst, HPC has long been applied mainly to act as catalyst for organic synthesis reactions or reagent for chemical analysis, few report has been given by now in the open literatures on its new application in gas purification. Kuznetsova and Yurchenko[3] studied the catalytic effect of the aqueous solutions of several HPC, PW₁₁M(H₂O)O₃₉⁵⁻ (M=Fe, Co, Ni), on the gas phase reaction of H₂S and O₂, they found that, under conditions of initial solution pH range from 5 to 7 and at temperature of 20 °C, only PW₁₁Fe(H₂O)O₃₉⁵⁻ has evident catalytic effect on the oxidation of H₂S by O₂. Yang and Chen[4] explored a two-step method of NO decomposition into N₂ using a solid state HPC as catalyst without reducing gas, the HPC they used was H₃PW₁₂O₄₀•6H₂O, it was shown that, at a space velocity of 5000h⁻¹, 70% of NO in a

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simulated flue gas is absorbed in the fixed bed at 150 °C, when the NO-saturated bed was heated to 450 °C, 68.3% of the absorbed NO is decomposed into N₂. Except the reports by the author[5-7], none has been given on the direct removal of H₂S from gas stream with the aqueous solution of HPC.

The HPC investigated in this study is H₄PVMO₁₁O₄₀, which can easily gain one or more electron when reacting with H₂S, making themselves changed into the reduction forms accordingly, the resultant HPC may be changed reversibly to their original form in the presence of air by losing the electron gained to oxygen. Hence, a circulating process of H₂S conversion with HPC can be formed in the presence of air. This is the principle of the new process for H₂S conversion.

There are two reasons for the author to introduce this newly developed method for H₂S removal. Firstly, the removal of H₂S from industrial gases is a key step for most industrial processes relevant to the direct utilization or further processing of gases, relating to which the new information especially new solution or technique is naturally needed for the improvement of gas industries. Secondly, although the new method is up-to-date, the devices it requires that of conventional, such as packed column, hence it can be readily industrialized provided the characteristics of the process are better understood.

2. Experimental

2.1. Absorbent and Gas

All chemicals used were of reagent grade and deionized water was used throughout. The feed gas of constant H₂S concentration, constant-flow rate is prepared by mixing two gas streams of dilute H₂S and pure nitrogen after passing through mass flow controller respectively, the mixed gas stream was analyzed by zinc acetate absorption-iodometric titration method to determine H₂S concentration.

2.2. Experimental Methods

The scheme of the experimental flow sheet can be found in literature[5]. With the combination of Pt electrode, calomel electrode and potential analyzer, dynamic redox potential detection was conducted to monitor the whole process of H₂S absorption with HPC and the resultant absorbent regeneration by air stream. In the meantime, online outlet H₂S concentration detection method was also executed with H₂S detector during the process of H₂S absorption. The concentration and rate of the inlet gas stream was controlled at a fixed value with two mass flow controllers. The operation temperature was controlled automatically by a thermostat at a fixed value. To compensate the water loss in the gas-liquid reactor owing to long time operation, the inlet gas stream was pre-humidified by passing through a water saturation tank. The desulfurization product was studied with the aid of Finber 1000 Energy Spectrum.

3. Results and Discussion

3.1. The Effect of HPC Concentration

To gas absorption, the absorbent concentration plays an important role in the whole process. Results from the effect of the absorbent concentration normally provide basic information for further design of the process equipment. From the experiment, we found a high dependence of the H₂S removal efficiency on HPC concentration, where HPC refers to H₄PVMO₁₁O₄₀. In details, the experiments were conducted under condition of: inlet gas, 0.31 l/min; absorption temperature, 30 °C; volume of the absorbent, 200 ml; H₂S concentration, 580 mg/m³. In Figure 1, the H₂S removal efficiency increases markedly as H₄PVMO₁₁O₄₀ concentration increases from 3.0×10⁻⁴ mol/l to 6.0×10⁻⁴ mol/l, and such tendency diminishes when H₄PVMO₁₁O₄₀ concentration increases further. Meanwhile, the adsorption curves tend to level off with time. These indicate that maintenance of desulfurization efficiency at high level as close to 90% requires using of absorbent with concentration higher than 2.5×10⁻³ mol/l, which is economically competitive compared to the iron chelate liquid redox absorbent for H₂S removal.

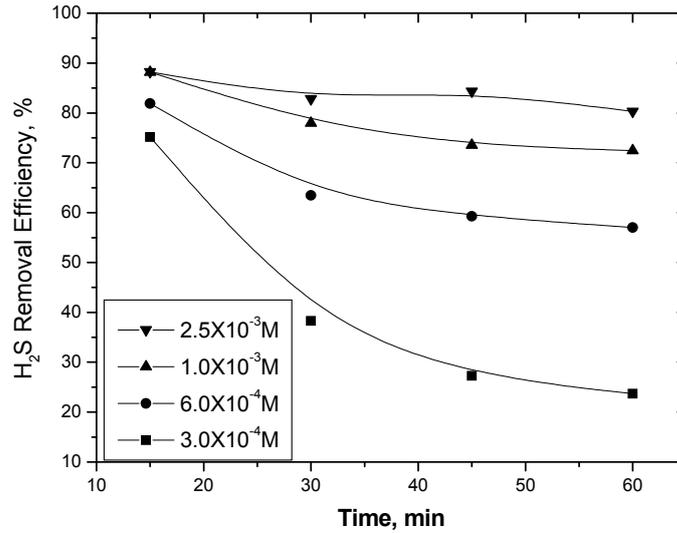


Fig. 1 Effect of $H_4PVMo_{11}O_{40}$ concentration on H_2S absorption

3.2. The Effect of Absorption Temperature

With other conditions remained unchanged, the effect of absorption temperature was examined. From the results shown in Figure 2, it can be found that the absorption curve locates within a quite stable position, showing slight tendency of being affected by the change in absorption temperature from 30 to 50 °C. This implies that application of such process requires less or no heat input to maintain favorable absorption temperature. If possible, ambient temperature is a good choice.

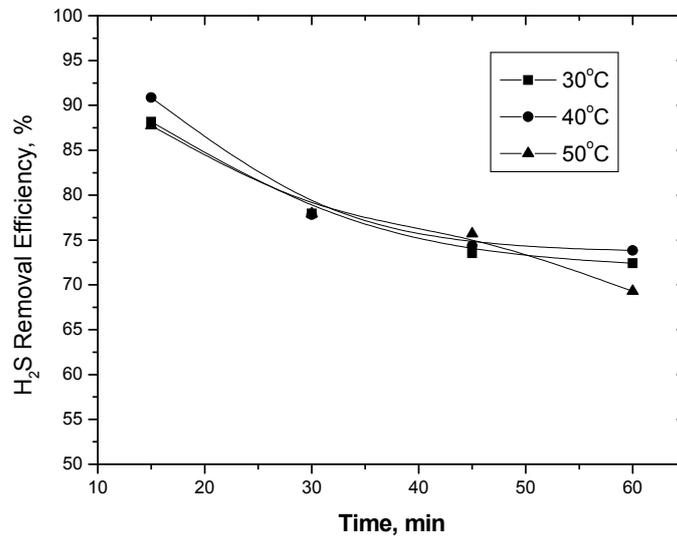


Fig. 2 Effect of temperature on H_2S absorption

3.3. The Effect of Inlet Gas H_2S Concentration

The effect of inlet gas H₂S concentration was examined under following conditions: inlet gas, 0.31 l/min; absorption temperature, 30 °C; volume of the absorbent, 200 ml; H₄PVMO₁₁O₄₀ concentration, 1×10⁻³ mol/l. The results (Fig.3) show that increasing inlet gas H₂S concentration from 571mg/m³ to 833 mg/m³ leads to a sharp decrease in H₂S removal efficiency while a quite less decline can be observed when inlet gas H₂S concentration increases from 419 mg/m³ to 571 mg/m³. These indicate that practical application should be cautious on the H₂S concentration in the gas to be treated, and H₄PVMO₁₁O₄₀ solution of 1×10⁻³ mol/l is applicable to treatment of gas containing H₂S of around 571 mg/m³ or lower.

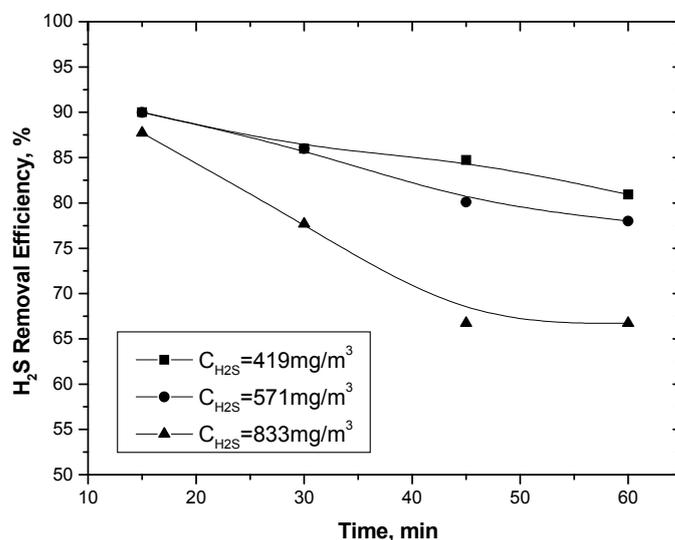


Fig. 3 Effect of inlet gas H₂S concentration on H₂S absorption

3.4. The Effect of Metal Sulfide Additive

To improve the desulfurization performance, many additives have been tested, from which metal sulfides have been found to be very effective. Shown in Table 1 are the test results on ZnS, CdS and CuS under the following experimental conditions: inlet gas, 0.50 l/min; absorption temperature, 30 °C; volume of the absorbent, 200 ml; H₄PVMO₁₁O₄₀ concentration, 1×10⁻³ mol/l; H₂S concentration, 580 mg/m³; additive/HPC=1:1, molar ratio; duration of the test, 30min. From the results listed in Table 1, it can be seen that the effect of metal sulfides follows the order of ZnS < CdS < CuS, where CuS shows the best enhancement effect on the absorption of H₂S.

Table 1 Test results on metal sulfides additives

	no additive	with ZnS	with CdS	with CuS
H ₂ S Removal Efficiency, %	83.63	84.73	88.71	100

Finally, energy spectrum analysis of the sedimentation products derived from 10 absorption-regeneration cycles with the absorbent systems of H₄PVMO₁₁O₄₀ was conducted under conditions of 15kV of accelerating voltage and 1×10⁻⁷A of electron beam current. We found that the composition of the sedimentation product is sulfur mainly, with little deposition compounds of molybdenum and vanadium.

4. Conclusions

The aqueous solution of H₄PVMO₁₁O₄₀ can be used as absorbent for H₂S removal. Among the three metal sulphides tested, CuS is the best for enhancing the performance absorbent. The desulfurization product is elemental sulfur mainly with little sedimentation of molybdenum and phosphorus.

5. Acknowledgements

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6. References

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